Micro-bioreactor array for controlling cellular microenvironments†

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High throughput experiments can be used to spatially and temporally investigate the many factors that regulate cell differentiation. We have developed a micro-bioreactor array (MBA) that is fabricated using soft lithography and contains twelve independent micro-bioreactors perfused with culture medium. The MBA enables cultivation of cells that are either attached to substrates or encapsulated in hydrogels, at variable levels of hydrodynamic shear, and with automated analysis of the expression of cell differentiation markers. The flow and mass transport in the MBA were characterized by computational fluid dynamic (CFD) modeling. The representative MBA configurations were validated using the C2C12 cell line, primary rat cardiac myocytes and human embryonic stem cells (hESCs) (lines H09 and H13). To illustrate the utility of the MBA for controlled studies of hESCs, we established correlations between the expression of smooth muscle actin and cell density for three different flow configurations.

Introduction

The cellular microenvironment, also termed a “cell niche”, controls and regulates stem cell fate.1,2 Historically, the term “niche” was used to describe the stem cell location,3 the components of the microenvironment surrounding the cells, and the biochemical or electrical signals produced by the support cells.4,5 The niche functions as a physical anchor and generates a number of extrinsic factors that control cell fate. From an engineering perspective, we may define the stem cell niche as a microenvironment with multiple regulatory factors, molecular and physical, that change in space and time and govern stem cell behavior. Replicating in vitro the “cell niche” normally found in vivo would likely help understand and ultimately control the signaling pathways that regulate cell fate, and help utilize the potential of stem cells in regenerative medicine.6–8 Each of the standard cell culture methods have advantages but also limitations. Well plates are easy to use, but they are suitable only for studies of molecular factors and cannot provide physical regulatory factors. Also, well plates operate essentially batch-wise, with the composition of medium constantly changing between the two medium replacements. In contrast, cell culture bioreactors can provide perfusion of medium,9–13 control medium composition and thereby support the cultivation of high cell densities, including cultures of human embryonic stem cells (hESCs)14,15 and embryoid bodies.16 However, the operating volumes of bioreactors are larger than those of well plates, which is a serious limitation in studies involving the use of expensive media components. Microscale approaches can potentially overcome both of these limitations.13,17–24

Soft lithography techniques, pioneered by Whitesides and colleagues,25 are inexpensive and relatively facile, and have found widespread application in bioseparation processes,26,27 micropatterning of cells and biomaterials,28,29 cell-based assays,30,31 and cell culture devices.32–34 Early applications of cell culture devices relate to hepatocytes where microscale features provide a reasonable analog for the microstructure of the liver.35 More recently, microfluidic platforms of interconnected chambers have been proposed as “living cell arrays” for studying gene expression36 and co-culture.21

In the existing microfluidic systems for stem cell differentiation, the individual chambers are not independent, as medium is distributed across one or more columns/rows of the array, leading to the cross-talk between the cells. By enclosing each chamber, this problem may be avoided, although it now becomes more difficult to control the individual chambers without resorting to an integrated valving system.13 Additionally, direct access to the cell growth surface makes it possible to apply coatings and uniformly seed the cells.

Here we propose micro-bioreactor arrays (MBAs) designed to address some of the limitations discussed above. MBAs are a hybrid between a bioreactor (represented by each individual culture well) and a microfluidic device (represented by the system providing independent flow of medium to each individual culture well). The MBA device combines the advantages of multi-well plates (small volume, high throughput, independent culture wells) and perfusion bioreactors (steady-state conditions, enhanced mass transport, application of physical signals). To take advantage of imaging compatibility of this device, we also developed an automated image
analysis routine that enables fast and unbiased analysis of nuclear and cytoplasmic differentiation markers.

We use the term “micro-bioreactor” because 12 culture wells, 3.5 mm in diameter × 2 mm deep, are located within a device that is the size of a microscope slide (26 × 76 mm). Two different configurations of the MBA were developed based on computational flow modeling and analysis of mass transport: MBA-bottom inlet/outlet (BIO; medium flows directly over the substrate with attached cells) and MBA-middle inlet/outlet (MIO; medium flows above the plane with the cells in a monolayer or encapsulated in hydrogel). These MBA configurations were validated for cultivations of the C2C12 cell line, primary rat cardiac myocytes and hESCs (lines H09 and H13). To illustrate the utility of the MBA for studies of hESCs, we established quantitative correlations between the density of hESCs differentiating into vascular lineages and the expression of smooth muscle actin.

**MBA design**

The design requirements for the MBA were: (1) high throughput experimentation with independent conditions for each bioreactor well, and low consumption of reagents and cells; (2) cultivation of cells in both the 2D setting (attached to a substrate) and three dimensional (3D) setting (encapsulated in hydrogel); (3) reproducible steady-state conditions in terms of cell density, medium composition, levels of oxygen and pH, flow regime, hydrodynamic shear and transport rates; (4) accurate spatial-temporal control of the cell environment; (5) in situ quantitative analysis of cell proliferation and differentiation, by automated image analysis of differentiation markers.

Fig. 1 shows the design of the system. The MBA is fabricated using soft lithography techniques, has the footprint of a standard microscope slide, and contains twelve independent culture wells. The constituent elements are shown in a top view (Fig. 1A): inlet (top, shown in red) and outlet (bottom shown in yellow) ports, culture wells (orange), gas exchangers (microfluidic channels between the inlet ports and the culture wells), stream splitters (divide single inlet/outlet streams by four), and the fluidic channels (connecting the inlets, gas exchangers, culture wells and outlets).

The microfluidic channels are 100 μm high by 100 μm wide. Gas exchangers (20 mm total length) are designed to equilibrate the oxygen level and pH in each of the three inlet streams of culture medium. A splitter then divides each of these streams into four equal parts, resulting in a total of twelve inlet streams leading into the twelve culture wells. In this way, each MBA has three inlet/outlet ports and three four-way splitters directing flow to the 4 × 3 array of culture wells. The total length of the fluid paths leading into each well is equivalent, and the pressure drop and velocity field are thus also equivalent for each of the culture wells.

The diameter of each culture well (3.5 mm) was selected to provide a small volume of medium (e.g., ~30 μl for BIO configuration) and the surface area (~10 mm²) large enough for a statistically significant number of cells to adhere (~10⁶). With standard soft lithography, the height of the micro-bioreactor chamber would be restricted to the thickness of the photoresist, generally between 50 μm and 200 μm. For our applications, this would result in three constraints: (i) limited access to the cell chamber for surface coating, cell seeding, and analysis, (ii) insufficient medium hold-up within the bioreactor chamber for cell survival without perfusion, and (iii) relatively high shear stresses for medium perfusion. For these reasons, we chose to work with an “open” microfluidic device where each chamber may be individually addressed (i.e., open) and has a height equal to that of device. A removable gas permeable membrane is used to enclose each chamber during experimentation.
Fig. 1B shows the two configurations of the MBA device that were used in the present study. Configuration BIO consists of a single layer of poly(dimethylsiloxane) (PDMS) with replica molded microfluidic channels and is perforated with an array of culture wells. The microfluidic channels are placed on the glass slide, such that the medium enters and exits the well at the bottom surface and flows directly over the attached cells (Fig. 1B, left).

Configuration MIO has an additional layer of PDMS, which (i) increases the depth of the culture well and (ii) presents medium inlets and outlets in the middle plane (Fig. 1B, right). As in the BIO configuration, the cells are cultured in a monolayer formed on the glass slide (with or without coating), with the main difference being a substantial reduction in exposure to hydrodynamic shear by culturing the cells outside the main plane of fluid flow. To accommodate the cultivation of hESCs in a 3D setting, a thin layer of photopolymerizing hydrogel may be added to the base of the wells in this configuration. Since cells in vivo are typically surrounded on all sides by extracellular matrix components, this approach more closely mimics the in vivo environment. The compressive stiffness of HA hydrogel can be varied from 0.5–50 kPa, by varying the concentration of HA and the level of crosslinking. The hydrogel layer experiences only a small level of shear stress; it is thin enough (typically 200–500 μm) to avoid major constraints in mass transfer and changes in flow patterns, yet thick enough for the cells to mimic some aspects of their native 3D environment.

The use of thin hydrogels and medium perfusion provides favorable conditions for encapsulation of hESCs in photo-polymerizable hydrogels. First, the high surface to volume ratio of hydrogel in the wells (20–50 cm² cm⁻³) allows for thin film (minimal light attenuation with depth) assumptions to be made. Also, medium perfusion efficiently removes any residual non-polymerized reactants.

The gas permeable membrane that seals each of the MBA chambers is held in place with a compression frame consisting of an aluminum frame, a clear polycarbonate cover, and four thumb screws (Fig. 1C). The experimental set-up is designed to assure steady state conditions during the dynamic culture. Each column of wells receives medium from one 10 ml syringe placed on ice (to minimize protein degradation) and is controlled with a syringe pump (Fig. 1D). Each outlet tube from the MBA was connected to a discharge medium collector placed ~20 cm above the device, all within the incubator.

Operating conditions: flow and mass transport

To characterize the operating conditions of the MBA, we evaluated the two configurations shown in Fig. 2B, in order to establish predictive flow and mass transport correlations for optimizing the conditions in the MBA. The large flow resistance within the 100 μm microfluidic channels ensures equivalence of flow conditions in the twelve individual micro-bioreactor wells of the MBA. At the entrance and exit of each well, the channel width is gradually increased to reach the diameter of the well (1 : 35 ratio of diameters, 1 : 20 ratio of heights), and minimize abrupt changes in fluid velocity. With the gradual change in the effective channel size and the dominance of viscous forces on the microscale, the flow field should remain laminar and uniform. Fluid flow was evaluated by solving the steady-state Navier–Stokes equations for incompressible fluid. The 3D solutions for the BIO and MIO configurations show that the pressure distribution within the chambers are uniform, with >99% of the pressure drop occurring at the inlet and the outlet to the chamber (Fig. 2 A–B). The uniformity of flow is further supported by the magnitude of the fluid velocity, which is very low throughout the culture well. In the BIO configuration, the fluid velocity in a plane 50 μm above the cell culture surface is less than 10 μm s⁻¹ over the entire surface area, and less than 3 μm s⁻¹ for 75% of the area (Fig. 2C). At these low flow rates, the shear stress is <0.01 dyn cm⁻². In the MIO configuration, the fluid velocity and shear stress are even lower (<0.01 μm s⁻¹, <0.0001 dyn cm⁻², Fig. 2D). These simulations show that both configurations operate at very low-shear, but with clear differences (two orders of magnitude) in the values of fluid velocity and hydrodynamic shear.

A semi-quantitative analysis of mass transport for each of the two flow regimes was performed for two representative molecules: oxygen (the most critical small molecule) and albumin (a molecule representative of large growth factors) (Fig. 2E–G). As expected, the thickness of the boundary layer was lower for the BIO configuration, and the mass transport coefficient was higher for oxygen than for albumin and higher for the BIO than for the MIO configuration. The Péclet number (Pe) is a measure of the relative contribution of convection with respect to diffusion. At Pe > 1, mass transport is dominated by convection, a situation associated with efficient exchange of nutrients and metabolites between the cells and culture media. In contrast, the dominance of diffusion (Pe < 1) may be associated with the accumulation of cell-secreted factors, hypoxia and changes in pH. The Pe numbers for the MIO configuration strongly suggest that diffusion dominates mass transport, whereas for the BIO configuration, convection plays a much larger role with diffusion only important for small molecules (oxygen) and negligible for large molecules. This analysis demonstrates the flexibility of an MBA approach for quantitative experimentation. Through simple regulation of flow rate, chamber height, and inlet/outlet configuration, a wide range of mass transport regimes are attainable.

Validation of the MBA for representative cell types: C2C12, rat cardiac myocytes and hESCs

To validate the utility of the MBA for controlled studies of cell growth and differentiation, we selected three model systems that are representative of the envisioned applications of this device: C2C12 myoblast cell line (MIO, BIO), primary cardiac myocytes derived from neonatal rat hearts (MIO, BIO), and hESCs (MIO). These cell types have well defined differentiation markers, and we have extensive experience in their use in various 2D and 3D configurations. Fig. 3 shows representative growth and differentiation data, at the time points characteristic for each cell type.

C2C12 cells readily adhered to the glass micro-bioreactor surface and formed spatially uniform monolayers with...
characteristically high cell densities over 7 days of culture (Fig. 3A, a–c). Close inspection of the chamber outlet channel revealed higher cell density with respect to the inlet channel due to cell migration along the velocity field line (Fig. 3A, c). This phenomenon was particularly noticeable within the 100 μm high outlet channel section of the MBA-BIO, where the average velocity and shear stress are high (~ 100 μm s\(^{-1}\) and ~0.1 dyn cm\(^{-2}\) at the flow rate of 10\(^{-6}\) ml s\(^{-1}\)). Within
7–10 days, cells formed multinucleated myotubes that were distributed throughout the culture well (Fig. 3A, d–e), elongated and expressed smooth muscle actin (Fig. 3A, e–f). Coating the chamber surfaces with collagen enabled neonatal rat cardiac myocytes to adhere and subsequently form spatially uniform monolayers (Fig. 3B, a–b). Cell viability, morphology and phenotype were well maintained, as seen by the expression of Troponin I. Spontaneous macroscopic contractions demonstrated that the cells were functionally active throughout the culture period.

The cultivation of hESCs turned out to be, as in most other systems, significantly more challenging than that observed for the other cell types. Similar to cardiac myocytes, hESCs required uniform collagen coating of the substrate to obtain even cell distribution (see Methods for details). The hESCs were also cultured encapsulated in a thin layer of hydrogel.
(hyaluronic acid, HA), a configuration that is 3D for the cells but effectively 2D from the perspective of the bioreactor operation.

For cultivation in a 2D setting (MIO), hESCs retained high viability with all conditions (data not shown). For cultivation in a 3D setting, medium perfusion affected the viability of all cells studied and most prominently the viability of hESCs (representative data for hESCs shown in Fig. 3B, c–d), presumably due to the combination of enhanced transport at the hydrogel surface and removal of any residual reagents from hydrogel polymerization. After 4 days of culture, the measured fractions of viable cells were 55 ± 10 and 67 ± 65 total cells for the static and perfused culture, respectively. To induce vascular differentiation of the HA-encapsulated hESCs, human vascular growth factor (hVEGF) was added to the culture medium, which resulted in extensive cell sprouting and α-smooth muscle actin (α-SMA) expression (Fig. 3B, e–f).

Taken together, these studies demonstrated that both MBA configurations (BIO, MIO, Fig. 1) support the growth and differentiation of healthy and viable cells.

Vascular differentiation of hESCs: effects of cell density and flow configuration on SMA expression

The MBA system was designed for live imaging of culture wells with optical and fluorescent microscopy. To take advantage of this option in studies of hESCs, we developed a simple automated system for image analysis that allows fast and unbiased analysis of cell growth and differentiation. Automated and semi-automated routines have been used to measure other biological parameters, such as the spindle length in a Drosophila cell line. The routine is similar, but not identical (measurements of the length vs. the numbers of positive cells). Fig. 4A shows a representative image of hESCs differentiating into vascular lineages and labeled for α-SMA (red), Oct4 (green) and DAPI (blue). A robust algorithm is used to assess the expression of nuclear and cytoplasmic markers in images of this kind.

To generate quantitative data, the positions of the individual cells stained with DAPI are first determined for a given view field. The expression of intranuclear (e.g., Oct4) and extranuclear markers is identified for each identified cell. Data are processed by a flow cytometer-like analysis, to obtain a dot plot or a histogram representing the intensity of a specific marker within the cell population. The present study used an automated routine to process images of hESCs cultured in three different flow configurations: static MBA (left column: a, d, g), perfused MBA-MIO (middle column: b, e, h) and MBA-BIO (right column: c, f, i), three different cell densities: 60 ± 6 (top row: a, b, c), 160 ± 4 (middle row: d, e, f) and 314 ± 15 (bottom row: g, h, i). Scale bars: 200 μm. (D) The fraction of differentiated cells was determined using the automated image analysis for each flow configuration for a range of cell densities observed over the time of the culture. Data are plotted as the fraction of hESCs expressing α-SMA as a function of the total number of cells in the field (an index of cell density) for each flow configuration. Vertical dotted lines correspond to the conditions in panels (C).

Fig. 4 Effects of cell density and flow configuration on hESC differentiation within the MBA device. (A) A representative merged image of cultured hESCs with immunofluorescent labels for α-SMA (red), Oct4 (green) and DAPI (blue). (B) Automated image analysis of cell differentiation. Individual cells are identified by nuclear staining (DAPI) and the coordinates of nuclei are stored in a data matrix. The presence or absence of a nuclear label (Oct4 is shown as an example) and cytoplasmic label (α-SMA is shown as an example) is identified for each identified cell. Data are processed by a flow cytometer-like analysis, to obtain a dot plot or a histogram representing the intensity of a specific marker within the cell population. (C) Examples of the immunofluorescence of SMA (red) and DAPI (blue) for hESCs cultured in three different flow configurations: static MBA (left column: a, d, g), perfused MBA-MIO (middle column: b, e, h) and MBA-BIO (right column: c, f, i), three different cell densities: 60 ± 6 (top row: a, b, c), 160 ± 4 (middle row: d, e, f) and 314 ± 15 (bottom row: g, h, i). Scale bars: 200 μm. (D) The fraction of differentiated cells was determined using the automated image analysis for each flow configuration for a range of cell densities observed over the time of the culture. Data are plotted as the fraction of hESCs expressing α-SMA as a function of the total number of cells in the field (an index of cell density) for each flow configuration. Vertical dotted lines correspond to the conditions in panels (C).
cytoplasmic (e.g., \( \alpha\)-SMA) markers is then tracked for each individual cell, and represented in the form of a histogram or a dot plot in a manner common to flow cytometry. Fig. 4B shows a schematic description of the developed imaging routine, which was utilized to probe the effects of cell density and flow regime on hESC differentiation.

hESCs were cultured using the MBA-BIO and MBA-MIO configurations, and a non-perfused MBA-BIO to serve as a static control. Cell density varied from \( 3 \times 10^2 \) to \( 3 \times 10^4 \) cells cm\(^{-2} \), corresponding to \( \sim 30 \) to 3000 cells per well. Vascular differentiation was evaluated by the expression of \( \alpha\)-SMA, using the imaging routine described above.

Fig. 4C shows representative images of cells stained for \( \alpha\)-SMA (red) and DAPI (blue), that were cultured using three different flow configurations (static, BIO and MIO). The top, middle and bottom rows of panels show images obtained for low, medium and high cell density (60 \( \pm \) 6, 160 \( \pm \) 4 and 314 \( \pm \) 15 cells per well, respectively).

In general, cells cultured in the MBA-BIO configuration (the one with a higher level of shear) exhibited higher levels of differentiation relative to the other two configurations (Fig. 4 C,D). This is consistent with the known role of hydrodynamic shear in vascular differentiation.\(^{44} \)

In all three configurations, the fraction of hESCs expressing \( \alpha\)-SMA increased as the cell density decreased (Fig. 4D). For example, in the MIO configuration, the percent of cells expressing \( \alpha\)-SMA decreased from \( \sim 23\% \) to \( \sim 2\% \) as the cell density increased from \( \sim 200 \) cells cm\(^{-2} \) to \( \sim 10000 \) cells cm\(^{-2} \). Cells cultured in the BIO configuration showed a similar trend, at higher expression levels of \( \alpha\)-SMA for comparable cell densities (Fig. 4D). Interestingly, Oct4 was not dependent on cellular density (data not shown). The fraction of the \( \alpha\)-SMA in hESC culture decreased linearly with the logarithm of cell density for all three bioreactor configurations. This graph summarizes the results from \( \sim 70 \) individual bioreactors for multiple MBA configurations. The automated assay for quantification of cell differentiation markers, presented here for the case of vascular differentiation of hESCs in 2D culture, could be extended to 3D cultures of cells and a variety of other differentiation markers.

This study demonstrated that the MBA could be used to study the effects of culture parameters on hESC differentiation, in a systematic manner and with only a minimal consumption of cells and reagents. The image processing routine used to assess the fractions of cells expressing differentiation markers (SMA and Oct4 in this case) can be considered an integral part of the proposed method.

**Application of MBA in studies of hESCs**

The MBA was designed to culture hESCs in a microarray setting, under controlled conditions, with imaging compatibility, and only minimal consumption of cells and reagents. hESCs are difficult to grow, require expensive medium and reagents, and from a biological perspective, their complex signaling networks and largely unknown regulatory factors often result in data variability. The use of a system that combines the advantages of microarrays (large numbers of groups and replicates, small volumes) and bioreactors (tight control of environmental conditions) with the automated routines of image processing to assess cell differentiation can largely improve the yield and quality of experimental data.

In general, the MBA shares many properties with other microfluidic-based platforms: low consumption of media, inexpensive fabrication, imaging compatibility, and high throughput. However, MBAs also provide close control of culture parameters (including hydrodynamic shear) in each culture well. Additional practical advantages include open access to the cell culture plane in each micro-bioreactor well, to ease surface coating, cell seeding and staining procedures. This allows for an easy translation of the existing biological protocols already established for hESCs to use in MBA formats, and a relatively straightforward use of existing liquid handling-robotic systems and microplate readers.

Notably, each MBA well maintains its own set of steady-state conditions via perfusion of culture medium in a single-pass mode, and without interaction with other wells within the same array. The medium at the outlet of each well is sent to the waste instead of being recirculated back to the cells (as in most perfused bioreactors). This way, there is no interaction between the wells, and the experiments are not confounded by paracrine signals being transferred downstream. In spite of single-pass flow, the consumption of medium is minimal because of the miniature size of the device. In studies of vascular differentiation of hESCs, 70 data points were generated over 4 days of culture using only 10 ml of medium.

One of our goals was to provide a uniform and controllable hydrodynamic environment for all cells in the culture chamber. The CFD-assisted design yielded two different configurations—MBA-BIO and MBA-MIO—which exhibit hydrodynamic shear stress that can be as low as \(<0.1\) and \(<0.001\) dyn cm\(^{-2} \), respectively. Both values are significantly below the threshold levels of shear stress that can affect the cells (1–5 dyn cm\(^{-2} \)), a feature very useful for cultivation of hESCs in a quiescent regime. On the other hand, if hydrodynamic shear is needed (e.g., to mediate cell differentiation) these levels can be increased by a simple increase of fluid velocity. Also, the BIO and MIO configurations provide different flow environments, and the experiments described above show that the culture of hESCs in a BIO configuration resulted in larger values of \( \alpha\)-SMA-positive cells than culture in the MIO configuration.

**Methods**

**Fabrication of the MBA**

The micro-bioreactor array was designed in a standard CAD program (SolidWorks, Concord, MA, USA), and then exported to Adobe Illustrator 9.0 (San Jose, CA, USA) for printing as a transparency mask (5080 dpi, PageWorks, Cambridge, MA, USA). The mask was used to prepare a 4" silicon wafer–SU-8 2100 master of the bioreactor image. The processing guidelines of the photoresist manufacturer were followed to achieve features with a uniform height of 100 \( \mu \)m.\(^{45} \)

The actual bioreactor layers were replica molded\(^{46,47} \) by pouring 35 ml of PDMS (Sylgard 184 Silicone Elastomer, Ellsworth Adhesives, Germantown, WA, USA) over a master
placed in a 150 mm Petri dish. Prior to this step, a thin layer of hexamethyldisilane (Fluka, Buchs, Switzerland) was vacuum deposited on the wafer surface to prevent adherence of the PDMS. The fluidic connection ports were punched through the PDMS with a 21-gauge stainless steel tube (0.635 mm ID, 0.81 mm OD, McMaster–Carr, Atlanta, GA, USA). In a similar manner, the micro-bioreactor wells were cored out using a 3.5 mm punch (Fray Products Corp., Buffalo, NY, USA), resulting in holes that were 3.35 mm in diameter. The layers of PDMS and glass were irreversibly bonded after treatment with vacuum gas plasma for 45 s (at 0.5 mbar and 50 W) (Harrick Scientific, Pleasantville, NY, USA). After coating the bottom surface of each well and seeding with cells, the entire bioreactor array was covered with a thin layer (0.2 mm) of PDMS. The MBA layers were held in place by mechanical compression via a frame consisting of an aluminium base, a polycarbonate cover, and four thumbscrews. Small lengths of stainless steel tubing (21-gauge, 10 mm length) were used to connect the MBA ports to soft Tygon tubing (0.8 mm ID, 2.4 mm OD, Cole Palmer, Vernon Hills, IL, USA). The medium flow rate was controlled via a syringe pump, with an accuracy of 0.1 μl min⁻¹ (PHD, Harvard Apparatus, Holliston, MA, USA). The culture medium was kept at 4 °C, while the entire MBA device was kept in an incubator (NAPCO, Winchester VA, USA) at standard conditions (37 °C, 95% humidity, 5% CO₂).

Hydrodynamic simulation

The Navier–Stokes equations for incompressible fluids were solved using Comsol Multiphysics software (Burlington, MA, USA) to obtain a flow field within the micro-bioreactor well for the BIO and MIO configurations. The 3D domain of the micro-bioreactor well was meshed using four-node tetrahedron finite elements with a maximum mesh size of 300 μm. Coarsening and refining of the mesh space grid ensured solutions independent of the spatial discretization.

The inlet boundary condition was set for a fully developed velocity profile (calculated on the basis of flow rate), while a zero pressure condition was imposed on the outlet and non-slip boundary condition set for channel and bioreactor walls. Assumption of longitudinal symmetry allowed solving the equations for only one half of the channel and chamber, thus minimizing computational time.

The medium viscosity and density values for DMEM medium with 5% FCS were taken from the literature. As a check on the validity of the simulation, the shear stress within the uniform rectangular channels was calculated from an approximation of the analytical solution for flow between parallel plates, \( \tau = 6\mu \frac{\dot{Q} b h}{b h^2} \) where \( \mu \) is the dynamic viscosity of the medium (0.0077 dyn s cm⁻²), \( \dot{Q} \) is the flow rate \( (5 \times 10^{-6} \text{ m s}^{-1}) \), \( b \) is the channel width (0.01 cm), and \( h \) is the channel height (0.01 cm). The calculated value of 0.058 dyn cm⁻² compares well to the result obtained by finite element modeling of the flow in the channel \( (~0.07 \text{ dyn cm}^{-2} \) at the position 0.32 cm from center of the well, Fig. 2C).

Mass transport calculations

To obtain concentration profiles within the micro-bioreactor wells for the BIO and MIO configurations, the mass balance equations for a convective diffusive regime were solved using Comsol Multiphysics software (Burlington, MA, USA). Fluid velocity profiles were obtained from the three dimensional solution. The concentration of 1 mM was used as a boundary condition at the inlet; zero concentration was imposed as a boundary condition at the cell surface. The Re and Pe numbers were then calculated using standard equations and literature values of diffusion coefficients for each solute.

Cell culture

C2C12 myoblast cells (murine, American Type Culture Collection) were grown to confluence in growth medium (DMEM with 20% fetal bovine serum, FBS). Cells were trypsinized, counted, and 2000 cells were added to each MBA well. After 12 h, medium perfusion was initiated at a flow rate of 0.3 μl min⁻¹ \( (0.432 \text{ ml day}^{-1}) \), which corresponds to 0.075 μl min⁻¹ per bioreactor. Perfusion medium contained low serum levels (2% FBS), to induce myogenic differentiation. Experimental methods with primary cells (cardiomyocytes) were similar to those with C2C12 line except that cells were seeded at 1000 cells per well and the culture medium contained 10% FBS. Details on cardiomyocyte isolation from 2-day old neonatal Sprague Dawley rats can be found elsewhere. Non-differentiated hESCs (lines H9 and H113; passage 20–35) (WiCell Research Institute, Madison, WI, USA) were grown on inactivated mouse embryonic fibroblasts (Chemicon International, Temecula, CA, USA) in growth medium consisting of 80% KnockOut DMEM, supplemented with 20% KnockOut Serum replacement, 4 ng ml⁻¹ basic Fibroblast Growth Factor, 1 mM l-glutamine, 0.1 mM β-mercaptoethanol, and 1% non-essential amino acid stock (all from Invitrogen Corp., Carlsbad, CA, USA). hESCs were passaged to a new feeder layer using 1 mg ml⁻¹ type IV collagenase (Invitrogen Corp., Carlsbad, CA, USA). For 3D studies, hESCs were removed from the feeder layer by incubation with collagenase for 20–30 min. For 2D studies, hESCs were removed from MEFs by incubation with EDTA (Promega), with 5% FCS, for 20 min, followed by separation into single cells using a 40 μm mesh strainer (Falcon). For 3D studies, the glass surface of each MBA chamber was treated with a solution of 4% 3-aminopropyltrimethoxysilane (Sigma–Aldrich, St. Louis, MO, USA) in acetone for 15 min. Each well was then coated with 0.05 mg ml⁻¹ collagen IV (R&D Systems, Minneapolis, MN, USA) for 1 h at room temp. The cells were seeded at concentrations of \( 10^5 \), \( 3 \times 10^5 \), \( 5 \times 10^5 \), and \( 10^6 \) cells per well. Medium perfusion was started 24 h after cell seeding to allow sufficient time for cell attachment.

Hydrogel preparation and hESC microencapsulation

For 3D studies, we utilized previously developed photo-crosslinkable methacrylated HA hydrogels. Recently showed that these HA hydrogels support the propagation of undifferentiated hESCs and the initiation of vascular differentiation. For hydrogel formation, methacrylated HA was dissolved in PBS containing 0.05 wt% 2-methyl-1-[4-(hydroxyethoxy)phenyl]-2-methyl-1-propanone (Irgacure 2959, I2959) and exposed to ultraviolet light (Black Ray, Redding, CA, USA) for 10 min. These encapsulation conditions have
previously been used for the encapsulation of a variety of mammalian cells.\textsuperscript{54}

hESCs were added to the precursor solution at a concentration of 0.5–1 × 10\textsuperscript{5} cells ml\textsuperscript{-1}. A volume of 30 μl of the cells–HA mixture was poured into each micro-bioreactor well, and photopolymerized (using ~10 mW cm\textsuperscript{-2} UV light, BlackRay) for 10 min. Cell–gel constructs were cultivated in growth medium (for proliferation), and endothelial cell medium (for differentiation) (PromoCell, Heidelberg, Germany). In some studies, medium was supplemented with 100 ng ml\textsuperscript{-1} hVEGF (R&D systems, Minneapolis, MN, USA).

**Immunofluorescence**

Cells were fixed in situ with accustain (Sigma–Aldrich, St. Louis, MO, USA) for 25 min at room temperature. Cells were stained for 1 h with the first antibody and then for 30 min with a secondary antibody, at room temperature. The wells were rinsed three times with PBS without calcium and magnesium (Invitrogen Corp., Carlsbad, CA, USA). DAPI (2 μg ml\textsuperscript{-1}; Sigma–Aldrich) was added to the last rinse. C2C12 cells were stained for monoclonal Tropomyosin (Sigma–Aldrich). hESCs were stained either for smooth muscle actin (1 : 20; Dako, Troy Michigan, USA), or Oct4 (1 : 50; R&D Systems, Minneapolis, MN, USA). For secondary staining, Cy3 or the FITC-conjugated antibody (1 : 50; Sigma–Aldrich, St. Louis, MO, USA) were used. Cardiomyocytes were stained for anti-rabbit Troponin I and the FITC-conjugated secondary antibody (both from Chemicon International, Temecula, CA, USA). The immuno-labeled cells were examined using a fluorescence microscope (Axiomat, Zeiss, Thornwood, NY, USA).

**Data acquisition and analysis**

The percent of differentiated and undifferentiated cells were evaluated by an imaging acquisition program written using scripts available in MATLAB, and MATLAB imaging toolbox (The MathWorks, Natick, MA, USA). Images of the entire area of the cell–gel construct were analyzed with the aid of automated transcription factors. The intensity of the cytoplasmic staining fluorescence was evaluated by considering the intensity of pixels within the ellipsoid corona centered in the nucleus and an area 50% bigger in size. Processed data were then used to count the number of cells and evaluate the fraction of cells expressing a specific marker. Graphical representation of data (dot plots, histograms) and statistical evaluation of signal intensities were performed by importing data into a free flow cytometry data analysis program (WinMDI 2.8).

**Conclusions**

Stem cell biology is increasingly relying on advanced technologies that provide better cell culture microenvironments and enable control over multiple molecular and physical regulatory signals. These enabling technologies are of particular interest to hESCs, because of the complexity of their regulatory pathways, and uncontrolled variables associated with traditional culture methods. We have developed a micro-bioreactor array that combines the advantages of microarrays with those of bioreactors, and provides a means to study the growth and differentiation of hESCs under controlled conditions and in a multiarray setting. The device is the size of a microscope slide and contains twelve independent micro-bioreactors perfused with culture medium. The design is flexible, as it allows 2D and 3D cell culture under variable levels of hydrodynamic shear and mass transport, which were characterized by computational methods. To demonstrate the operation of the MBA, we cultured C2C12 cells, rat cardiac myocytes and hESCs within the system. A system for automated in situ image analysis of the expression of cell differentiation markers has also been developed and used to investigate the effects of cell density and flow regime on vascular differentiation of hESCs. This device can thus serve as a tool for studying hESCs in the context of their environment.

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